

Effect of a micro-structure on the thermal striping damage of an edge-cracked slab

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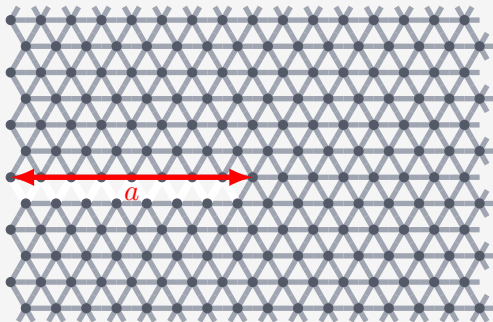
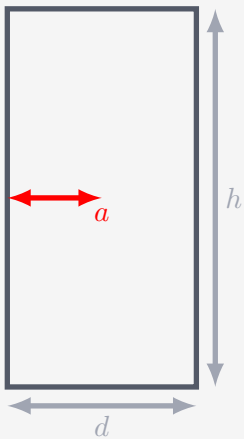
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The thermally striped geometries



The uncoupled thermoelastic problem

In the continuum

$$\begin{aligned} \mathcal{L}U(\mathbf{x}; t) &= \alpha(3\lambda + 2\mu)\nabla T(\mathbf{x}; t), & \mathbf{x} \in \Omega \setminus M_a, \\ \boldsymbol{\sigma}^{(n)}[U](\mathbf{x}; t) &= \alpha(3\lambda + 2\mu)\mathbf{n}T(\mathbf{x}; t), & \mathbf{x} \in B_0 \cup B_d \cup M_a^+ \cup M_a^-, \\ U(\mathbf{x}; t) &= \mathbf{0}, & \mathbf{x} \in \{\mathbf{x} : 0 < x_1 < d, |x_2| = h/2\}. \end{aligned}$$

In the discrete elastic lattice

$$\begin{aligned} \sum_{\mathbf{q} \in \mathcal{C}(\mathbf{p})} [B(\mathbf{q}) \{ \mathbf{u}(\mathbf{p} + \mathbf{q}; t) - \mathbf{u}(\mathbf{p}; t) \} \\ - \frac{\alpha\ell}{2} \mathbf{b}(\mathbf{q}) \{ \Theta(\mathbf{p} + \mathbf{q}; t) + \Theta(\mathbf{p}; t) \}] = \mathbf{0}, & \quad \mathbf{p} \in \Gamma, \\ \mathbf{u}(\mathbf{p}; t) = \mathbf{0}, & \quad \mathbf{p} \in \gamma_h. \end{aligned}$$

The heat conduction problem

In the continuum

$$\begin{aligned}
 \kappa \Delta \theta(\mathbf{x}) &= i\omega \theta(\mathbf{x}), & \mathbf{x} &\in \Omega, \\
 \theta(\mathbf{x}) &= T_0, & \mathbf{x} &\in \Omega \cap \{\mathbf{x} : x_1 = 0\}, \\
 \theta(\mathbf{x}) &= 0, & \mathbf{x} &\in \Omega \cap \{\mathbf{x} : x_1 = d\}, \\
 \nabla[\theta(\mathbf{x})] \cdot \mathbf{p} &= 0, & \mathbf{x} &\in \Omega \cap \{\mathbf{x} : |x_2| = h/2\}.
 \end{aligned}$$

In the discrete lattice

$$\begin{aligned}
 \vartheta(\mathbf{p}) &= \frac{1}{i\omega \Xi + |\mathcal{N}(\mathbf{p})|} \sum_{\mathbf{q} \in \mathcal{N}(\mathbf{p})} \vartheta(\mathbf{p} + \mathbf{q}), & \mathbf{p} &\in \Gamma, \\
 \vartheta(\mathbf{p}) &= T_0, & \mathbf{p} &\in \gamma_0, \\
 \vartheta(\mathbf{p}) &= 0, & \mathbf{p} &\in \gamma_d, \\
 \vartheta(\mathbf{p}) &= \frac{1}{|\mathcal{N}(\mathbf{p})|} \sum_{\mathbf{q} \in \mathcal{N}(\mathbf{p})} \vartheta(\mathbf{p} + \mathbf{q}), & \mathbf{p} &\in \gamma_h.
 \end{aligned}$$

An effective stress intensity factor for the lattice

For a sufficiently refined lattice the vertical displacements behind the crack tip exhibit similar asymptotic behaviour to the continuum.

$$u_2(\mathbf{p}) \sim \frac{K_I^{(\text{eff})}}{(1-k^2)\mu} \sqrt{\frac{a-x_1(\mathbf{p})}{2\pi}} + b_1 [a-x_1(\mathbf{p})] + b_2 [a-x_1(\mathbf{p})]^{3/2} + b_3 [a-x_1(\mathbf{p})]^2,$$

where $k = 3 - 4\nu$ and μ is the shear modulus corresponding to the homogenised continuum.

For the continuum, it is convenient to use a modified J -integral to compute the Stress Intensity Factor.

$$\frac{1-\nu^2}{E} K_I^2 = \frac{1}{2} \int_{\gamma} \left(\sigma_{ij} \epsilon_{ij} - \frac{E\zeta}{1-2\nu} T \epsilon_{ii} \right) dx_2 - \int_{\gamma} \sigma_{ij} n_j \frac{\partial U_i}{\partial x_1} ds + \frac{E\zeta}{1-2\nu} \int_{\Gamma} \epsilon_{ii} \frac{\partial T}{\partial x_1} dA$$

